



Agenda and Objectives



Trane Engineers Newsletter Live Series Upgrading Existing Chilled-Water Systems

The discussion for upgrading a chilled-water system begins for several reasons: repurposing a building, reducing energy use or replacing outdated equipment to name a few. A U.S. DOE-funded study concluded that commissioning is indeed cost-effective for both new and existing buildings with potential energy cost savings of over \$18 billion.

This course will provide designers with specific strategies for chiller upgrades, optimization or replacement. We'll also discuss reusing components of a chilled-water system and identify control upgrades that are often beneficial.

By attending this ENL you will be able to:

1. Identify opportunities to upgrade or repurpose chillers
2. Apply various design strategies and compare the energy-saving opportunities they offer existing systems
3. Apply the use of variable flow in existing systems
4. Identify and apply control strategies to optimize and reduce system energy use and lower energy costs

Agenda

- 1) Overview
 - a) Repurposing a building
 - b) Remove false loads
 - c) Retune/recommission
- 2) Change the chiller
 - a) Retrofit (incentives, drive, free cooling, reselection)
 - b) Replace
- 3) Select different design parameters
 - a) Expand on use of additional lift (how it's supposed to run)
 - b) Retrofit chilled-water opportunities
 - c) Retrofit condenser water opportunities
- 4) Change system configuration
 - a) Primary-secondary
 - b) Variable primary/variable secondary
 - c) VPF
 - d) Unit control retrofits
 - e) Ice
- 5) Enhanced controls
 - a) How many chillers to operate
 - b) Pump pressure optimization
 - c) Chiller tower optimization
 - d) VFD tower
 - e) Variable condenser water flow
- 6) Summary, resources

Trane Engineers Newsletter Live Series
Upgrading Existing Chilled-Water Systems
(2011)

Susanna Hanson | applications engineer | Trane

Susanna is an applications engineer at Trane with over eleven years of experience with chilled-water systems and HVAC building load and energy analysis. Her primary responsibility is to aid system design engineers and Trane personnel in the proper design and application of HVAC systems. Her main areas of expertise include chilled-water systems and ASHRAE Standard 90.1. She is also a Certified Energy Manager.

She has authored several articles on chilled water plant design, and is a member of ASHRAE SSPC 90.1 Energy Standard for Buildings Except Low-Rise Residential Buildings. Susanna earned a bachelor's degree in industrial and systems engineering from the University of Florida, where she focused on building energy management and simulation.

Mick Schwedler, PE | manager, applications engineering | Trane

Mick has been involved in the development, training, and support of mechanical systems for Trane since 1982. With expertise in system optimization and control (in which he holds patents), and in chilled-water system design, Mick's primary responsibility is to help designers properly apply Trane products and systems. To do so, he provides one-on-one support, writes technical publications, and presents seminars.

Mick is the immediate past Chair of SSPC 90.1, which was responsible for writing ANSI/ASHRAE/IESNA 90.1-2007, a prerequisite for LEED. He also contributed to the ASHRAE GreenGuide and is a former member of the LEED Energy and Atmospheric Technical Advisory Group (TAG). Mick earned his mechanical engineering degree from Northwestern University and holds a master's degree from the University of Wisconsin Solar Energy Laboratory.

Bonnie Spalding | service products manager | Trane

Bonnie joined Trane in 2004 as a Marketing Engineer for the Rental Services business. Currently she manages the Trane Service Products group, the team responsible for providing chiller upgrade and retrofit products including refrigerant conversions, purges, AdaptiView controls, frequency drives, CenTraVac motors and starters. The primary goal of her team is to help building owners/operators reduce HVAC operating costs through modernization of their chillers.

Prior to Trane she spent 15 years in engineering, sales, and marketing within the Ingersoll Rand air compressor business. Bonnie earned her Bachelor of Science degree in Mechanical Engineering from University of North Carolina at Charlotte.

Upgrading Existing Chilled-Water Systems



**EDUCATION
PROVIDER**

Ingersoll Rand

is a USGBC Education Provider committed to enhancing the professional development of the building industry and LEED Professionals through high-quality continuing education programs.

As a USGBC Education Provider, we have agreed to abide by USGBC-established operational and educational criteria, and are subject to course reviews and audits for quality assurance.



Approved for **1.5** GBCI CE Hours for LEED Professionals.



"Trane" is a Registered Provider with The American Institute of Architects Continuing Education Systems. Credit earned on completion of this program will be reported to CES Records for AIA members. Certificates of Completion for non-AIA members available on request.

This program is registered with the AIA/CES for continuing professional education. As such, it does not include content that may be deemed or construed to be an approval or endorsement by the AIA of any material of construction or any method or manner of handling, using, distributing, or dealing in any material or product. Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.

Copyrighted Materials

This presentation is protected by U.S. and international copyright laws. Reproduction, distribution, display, and use of the presentation without written permission of Trane is prohibited.

© 2011 Trane, a business of Ingersoll Rand. All rights reserved.

upgrading existing chilled-water systems

What You'll Learn...

- Strategies for chiller upgrades, optimization or replacement
- How to apply various design strategies
- Apply the use of variable flow in existing systems
- Identify and apply control strategies to optimize and reduce system energy use and lower energy costs.

Agenda

- Motivation for upgrade, replacement
- Upgrading existing chillers
- Repurposing chillers
- Retrofitting the chilled water system
- Control upgrades
- Condenser-side opportunities

Today's Presenters



Bonnie Spalding
Service Products Manager

7 | © 2011 Trane, a business of Ingersoll Rand

Today's Presenters



Mick Schwedler
Applications
Engineering Manager



Susanna Hanson
Applications
Engineer

8 | © 2011 Trane, a business of Ingersoll Rand

Overview

- What prompts an upgrade?
 - System not working well anymore
 - Building repurposed or loads reduced
 - Re-commissioning for efficiency, other benefits
 - Existing buildings: median 15% cost savings, payback 0.7 years
 - New buildings: median payback period 4.8 years
 - Widespread commissioning of existing commercial buildings could save the nation over \$18 billion a year in energy costs alone

Source: <http://eetd.lbl.gov/emills/PUBS/Cx-Costs-Benefits.html>

What's Not Working

- Equipment aged out or requires too much maintenance
- Out of capacity
- Energy bills are too high

Building Repurposed

- Space use classification changes
- Tenants attracted and retained by operation, comfort
- Process or manufacturing loads added or removed

Reduce Loads

Remove load before modifying chilled water system

- Lighting retrofits, local or task lighting addressed
- Envelope retrofits (windows, doors, insulation, etc.)
- Localized heating and cooling removed or reduced
- Items identified in an energy audit

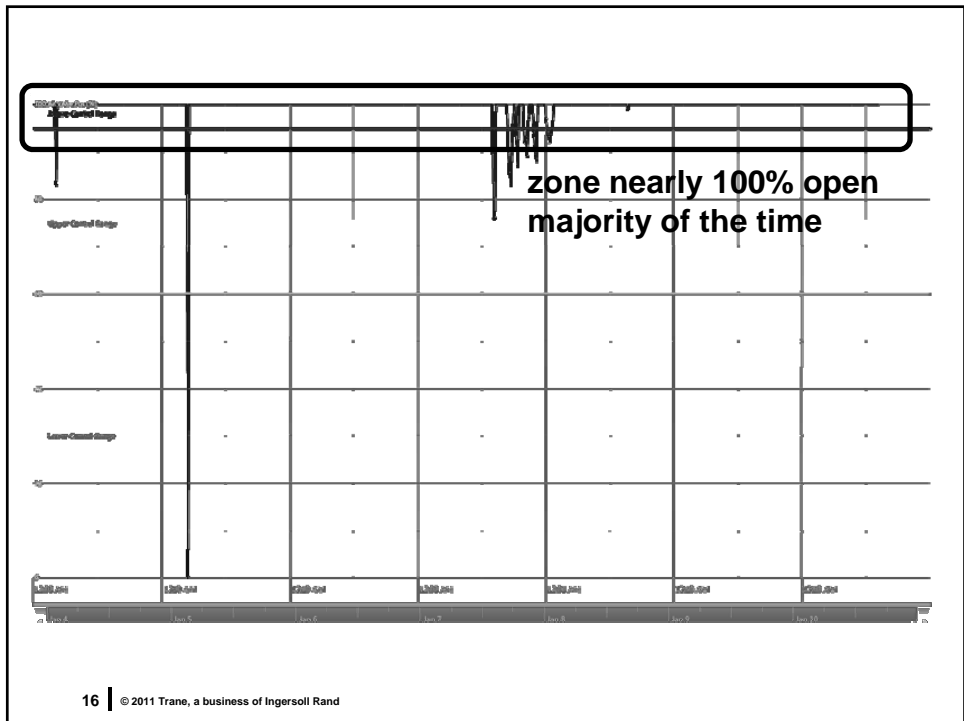
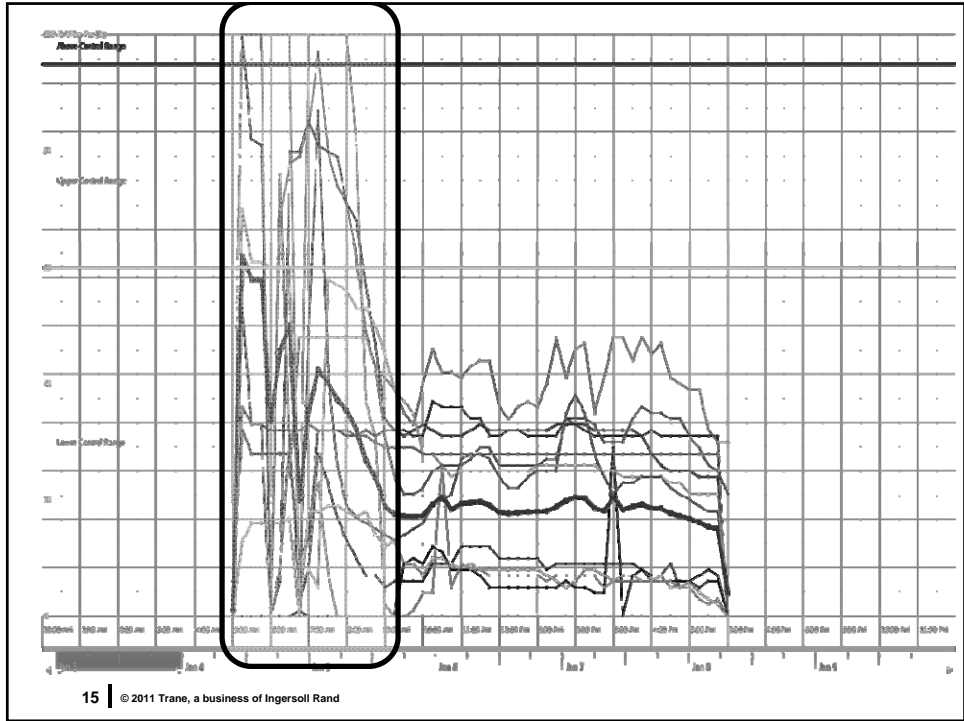
Reduce Loads

- Simultaneous heating and cooling
 - Stuck or broken valves
 - Leaky return dampers
- Control issues
 - Rogue zones
 - Zones that are rarely or never satisfied hinder system control algorithms
 - Overrides
 - Temperature
 - Flow
 - Schedule

Retune or Recommission

- Does the system work well as it was designed?
- Does the system as designed not work well?

- What modes of operation are working/not working?
- What triggered the problem?
- Can control be improved?



Retune or Recommission

- Does the system work well as it was designed?
- Does the system as designed not work well?

- What modes of operation are working/not working?
- What triggered the problem?
- Can control be improved?
- **System size truly the problem—what can be done?**

Chiller Upgrade Options

- Replace the chiller
 - Size the new chiller properly
 - Compare new chiller options
 - Variable speed drive
 - High efficiency
- Retrofit with a drive
- Comply with ASHRAE 90.1



Upgrading Existing Chilled-Water Systems



Chiller Replacement

Replace the Chiller

- High efficiency or drive?
 - Incentives?
- Conservatism factor
 - Lift or tons?
- Expanded lift or capacity reselection
 - Pipes are usually unchanged
 - Space for towers may be limited
 - Simultaneous heating and cooling (heat recovery?)
 - Escalating on-peak energy or demand charges (ice or reduced peak kW from chiller)

air-cooled chillers
ASHRAE 90.1

Capacity (tons)	2007		2010	
<150	9.562	EER	9.562	EER
	10.416	IPLV	12.500	IPLV
≥ 150	9.562	EER	9.562	EER
	10.416	IPLV	12.750	IPLV

- Positive displacement chillers evaluated at AHRI Standard 550/590 “standard” conditions (there is no derate for non-standard conditions)

water-cooled positive displacement chillers
ASHRAE 90.1

Capacity (tons)	2007	2010 Path A	2010 Path B
<75		0.780	0.800
	0.790	0.630	0.600
≥ 75 and < 150	0.676	0.775	0.790
		0.615	0.586
≥ 150 and < 300	0.717	0.680	0.718
	.0627	0.580	0.540
≥ 300	0.639	0.620	0.639
	0.571	0.540	0.490

- Positive displacement chillers evaluated only at AHRI Standard 550/590 “standard” conditions

water-cooled centrifugal chillers
ASHRAE 90.1

Capacity (tons)	2007		2010 Path A		2010 Path B	
	Full Load	IPLV	Full Load	IPLV	Full Load	IPLV
<150	0.703	0.669				
≥ 150 and < 300	0.634	0.596	0.634	0.596	0.639	0.450
≥ 300 and < 600	0.576	0.549	0.576	0.549	0.600	0.400
≥ 600	0.576	0.549	0.570	0.539	0.590	0.400

- requirements must be adjusted for “non-standard” conditions

centrifugal chiller nonstandard adjustment
ASHRAE 90.1

- Full load requirement = Table FL / kAdj
- NPLV requirement = Table IPLV / kAdj
- Kadj = A * B where
 - $A = 0.00000014592 * (\text{LIFT})^4 - 0.0000346496 * (\text{LIFT})^3 + 0.00314196 * (\text{LIFT})^2 - 0.147199 * (\text{LIFT}) + 3.9302$
 - $\text{LIFT} = \text{LvgCond} - \text{LvgEvap}$
 - $\text{LvgCond} = \text{Full-load condenser leaving water temperature (°F)}$
 - $\text{LvgEvap} = \text{Full-load leaving evaporator temperature (°F)}$
 - $B = 0.0015 * \text{LvgEvap} + 0.934$
- Applicable over the following full-load design ranges:
 - Minimum Leaving Evaporator Temperature: 36°F
 - Maximum Leaving Condenser Temperature: 115°F
 - $\text{LIFT} \geq 20^\circ\text{F}$ and $\leq 80^\circ\text{F}$

Chiller Replacement

- Correctly size the new chiller
 - Determine actual building load
 - Downsize chiller if possible
 - Upsizing? Higher efficiency to reuse electrical service

Chiller Size	Chiller Efficiency	Electrical Service
400 tons	0.68 kW/ton	272 kW
550 tons	0.50 kW/ton	275 kW
550 tons with VFD	0.57 kW/ton	314 kW
Max Chiller Size	Chiller Efficiency	Electrical Service
574 tons with VFD	0.53 kW/ton	300 kW
600 tons	0.50 kW/ton	300 kW

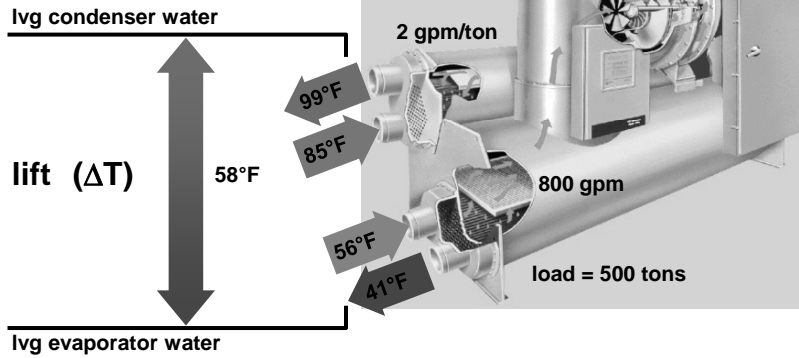
25 | © 2011 Trane, a business of Ingersoll Rand

Chiller Replacement

- Correctly size the new chiller
 - Determine actual building load
 - Downsize chiller if possible
 - If more chiller capacity is needed, higher efficiency reduces need for expanding electrical service
- Replace with higher efficiency chiller
 - Reduce demand and consumption
 - Constant speed or variable speed?

26 | © 2011 Trane, a business of Ingersoll Rand

Lift Versus Load



$$\text{load} \propto \text{gpm} \times (T_{\text{ent evp}} - T_{\text{lvg evp}})$$

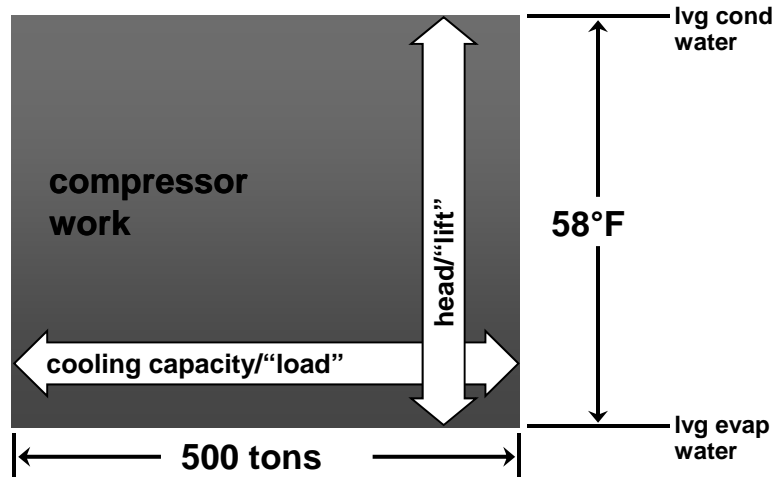
$$\text{lift} \propto P_{\text{cnd}} - P_{\text{evp}}$$

$$\text{lift} \propto T_{\text{lvg cnd}} - T_{\text{lvg evp}}$$

© 2008 American Standard Inc.

27 | © 2011 Trane, a business of Ingersoll Rand

Compressor Work and Chiller Efficiency

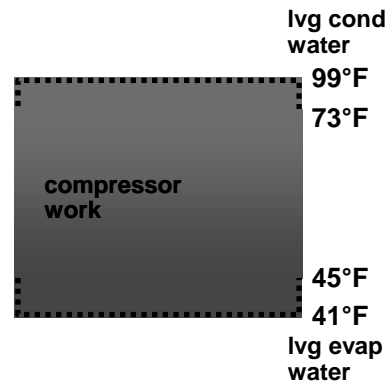


© 2008 American Standard Inc.

28 | © 2011 Trane, a business of Ingersoll Rand

Lessons Learned

- To reduce lift:
 - Decrease condenser pressure by reducing leaving-tower water temperature
 - Increase evaporator pressure by raising chilled water setpoint
- VSDs optimize chiller lift efficiency



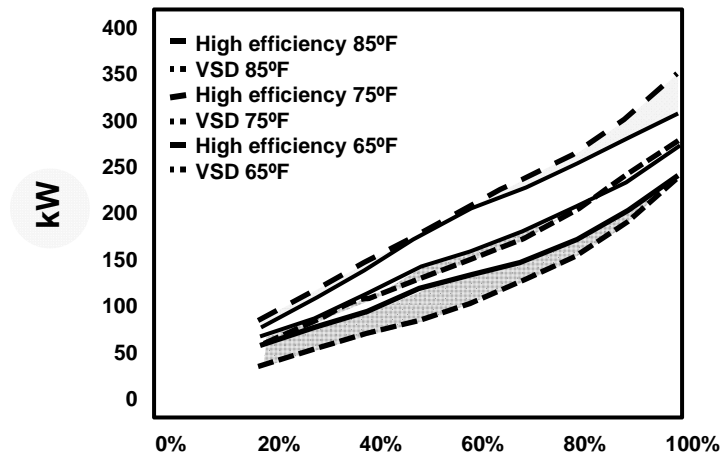
constant or variable speed? Chiller Replacement

- Compare same price VSD chiller and higher full load efficiency chiller
 - Make sure each chiller meets ASHRAE 90.1 full and part-load requirements
- Use comprehensive analysis to determine which to purchase

same-price chiller
Example Performance

Option	Full Load (kW/ton)	IPLV (kW/ton)
VSD	0.572	0.357
High Efficiency	0.501	0.430

same-price chiller
Example Performance



same-price chiller
Observations

- At high condenser water temperatures, constant speed is more efficient
- At low condenser water temperatures (low lift), variable speed is more efficient
- Analysis is required
 - Load and condenser water temperature do not vary directly with one another
 - Account for loads at different ECWT

guidance
VSD or High Efficiency?

- High efficiency
 - Significant demand charges
 - Humid climates
 - Multiple chillers in the plant
 - Economizer that reduces low load/low lift operating hours
- VSD
 - Many hours at low condenser water temperature—and low load
 - Perhaps only on one chiller
 - Factor in replacement of VSD when performing life cycle assessment

Upgrading Existing Chilled-Water Systems



Chiller Retrofits

Chiller Upgrade Options

- Comply with ASHRAE 90.1
- Replace the chiller
 - Size the new chiller properly
 - Compare new chiller options
 - Variable speed drive
 - High efficiency
- **Retrofit**
 - **Add a variable speed drive**
 - **Re-select**
 - **Field modifications**

Add VSD to Existing Chiller

- Comply with ASHRAE 90.1 requirements for retrofits
 - Ensure that modification will not result in an increase in annual energy consumption
- Controls updates if necessary or beneficial
- Perform return on investment analysis
- Understand how a drive may benefit chiller performance

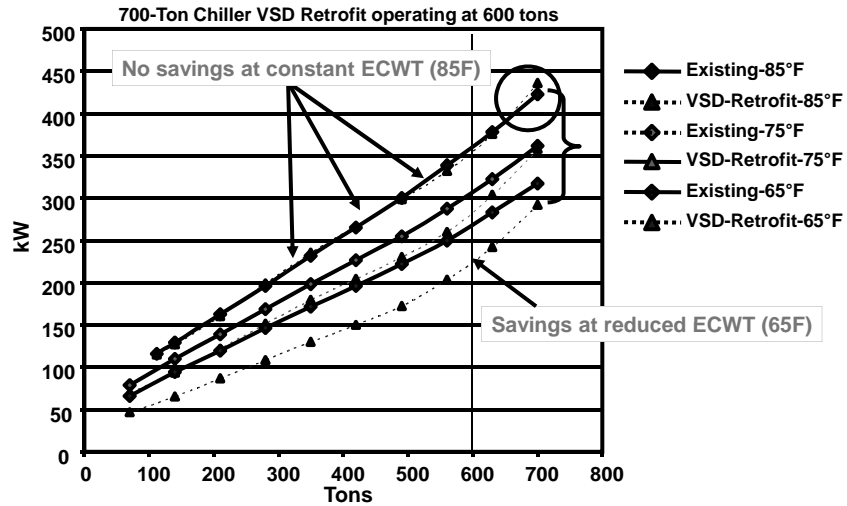
37 | © 2011 Trane, a business of Ingersoll Rand

VSD Existing Chiller Performance

- Demand rises 2–4% at design conditions
- Largest benefit at lower condenser water temperatures
- Corrects for improper impeller sizing
 - Due to original design conservatism
 - Due to changes in loads
 - Due to other duty changes
 - Ice builder now in normal cooling line-up
 - Heat recovery not needed all the time
 - Series chiller conversion from parallel

38 | © 2011 Trane, a business of Ingersoll Rand

drive impact
Existing Chiller Performance



drive retrofit
Issues to Consider

Utility rates?
 Demand Charge?
 Ratchet?

- VSD efficiency loss at full load
- If chiller was oversized the demand may be lower

How often will it operate at advantageous conditions?

- 24/7 operation may be beneficial
- Economizer reduces the loads at advantageous conditions

drive retrofit
Issues to Consider

How much energy is consumed by the cooling tower?

- Need to balance tower and chiller energy
- Is tower retrofit also needed

Is the chiller oversized for the load?

- Load reduction in conjunction with reduced CW temperatures may offer significant savings

rate of return
Return on Investment

- Investment
 - First costs
 - Incentives
- Annual operating costs
 - Calculated savings
- Life-cycle cost analysis
- Payback

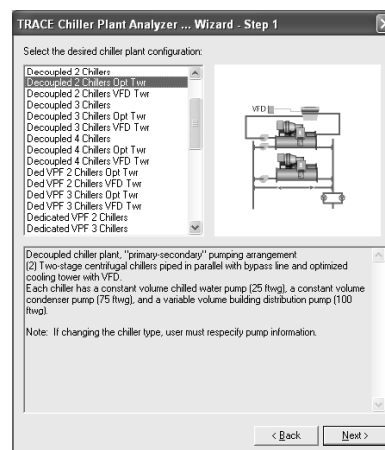
Financial Incentives

- Government
 - Tax incentives
 - Corporate, property, sales
 - Grants
- Utility
 - Rebates
 - Rate discounts
 - Low/no interest loans
- Resource:
 - DSIRE (Database for State Incentives for Renewables & Efficiency) found at dsireusa.org

Annual Operating Costs

Energy Savings Modeling

- Peak cooling load
- Simultaneous
 - Weather data
 - Building profile
 - Building location
- Operational hours
- Economizer capabilities
- Auxiliary energy
- Actual utility rates



Chiller Upgrade Options

- Comply with ASHRAE 90.1
- Replace the chiller
 - Size the new chiller properly
 - Compare new chiller options
 - Variable speed drive
 - High efficiency
- **Retrofit**
 - **Add a variable speed drive**
 - **Re-select**
 - **Field modifications**

Re-select/Renew

When planning to overhaul chiller consider:

- Re-selecting for current operating parameters
 - Best efficiency for new load conditions
 - Trim or replace impellers on centrifugal chiller
 - Ice making—adding glycol
 - Adding heat recovery to air cooled chiller
- Re-tubing if considerable number plugged or plugging
 - More efficient designs available
 - Renew to original efficiency
- Remanufactured motor—make sure inverter compatible
- Investing in labor already so be sure to optimize retrofit opportunities

Overhauled Chillers



47 | © 2011 Trane, a business of Ingersoll Rand

Chiller Retrofit Summary

- Several options available
- Take advantage of significant maintenance activities to maximize the labor content
- Look at ROI
 - First and life cycle costs
 - Potential savings
 - Incentives
- Evaluate independently and in conjunction for best ROI
- Know where your building load is going

48 | © 2011 Trane, a business of Ingersoll Rand

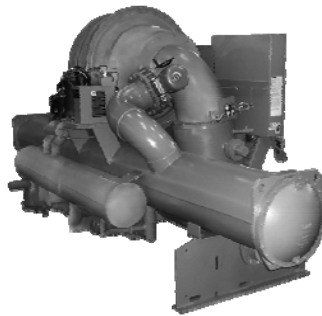
Upgrading Existing Chilled-Water Systems



Chiller Reselections

Free Cooling

- On the CTV chiller
 - Refrigerant migration
- Upstream of the chiller
 - Heat exchanger
 - Dry cooler
(with air-cooled chiller)



Existing Air-cooled Chiller

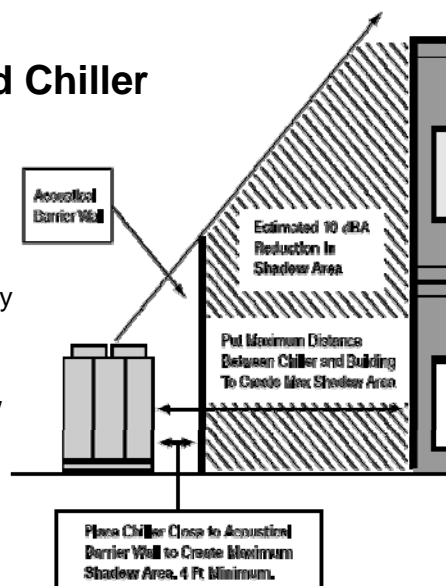
- Add ice storage
 - Centrifugal-like performance
 - “Right sizes” an undersized or oversized system
 - Saves energy and energy cost



51 | © 2011 Trane, a business of Ingersoll Rand

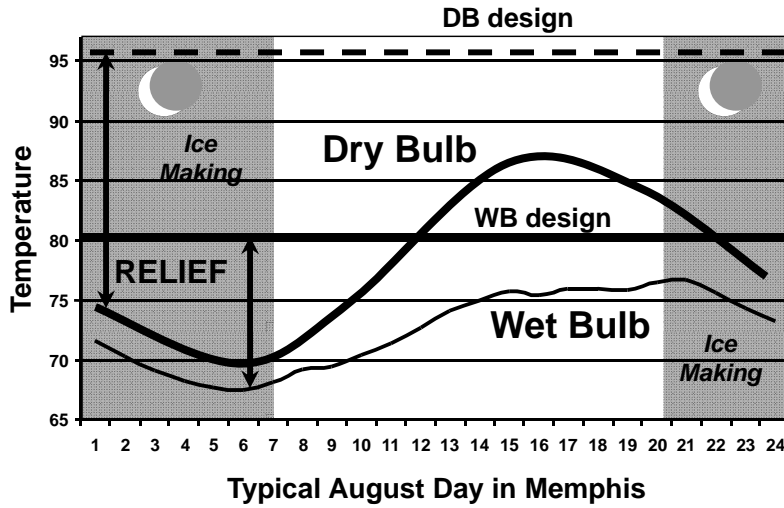
Existing Air-cooled Chiller

- Consider acoustic attenuation
 - What is the neighborhood?
- Finish ice production quickly
 - Easier to do in the shoulder months
- Consider condenser airflow when constructing walls



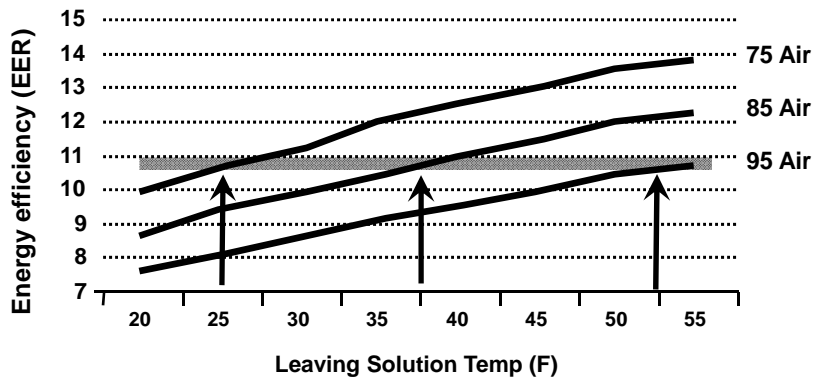
52 | © 2011 Trane, a business of Ingersoll Rand

Condenser Relief



53 | © 2011 Trane, a business of Ingersoll Rand

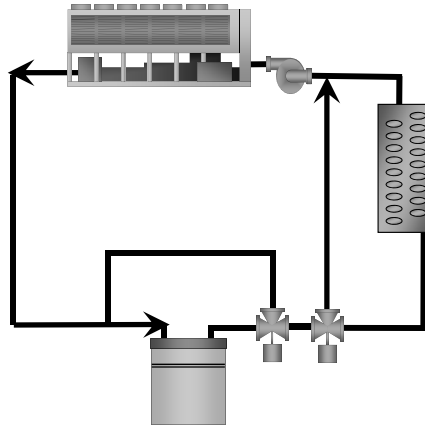
EER Leaving Solution Temp and Ambient Relief



54 | © 2011 Trane, a business of Ingersoll Rand

Simple Air-cooled Chilled Water System

- Chiller
- Downstream ice tanks
- Blending valve
- Diverting valve
- Controls
- Heat transfer fluid

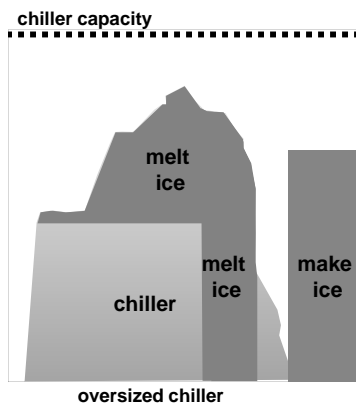


55 | © 2011 Trane, a business of Ingersoll Rand

Right-sizing with Ice and Existing Chillers

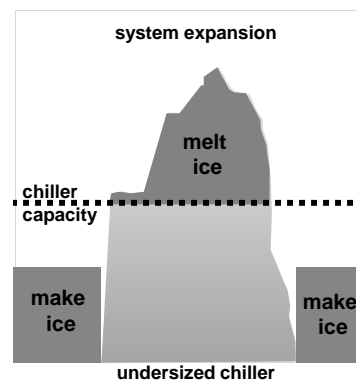
Full storage or oversized chiller

- Short on-peak windows
- Good rebates available



Partial storage or undersized chiller

- Reduces peak demand
- Shifts load to more efficient time



56 | © 2011 Trane, a business of Ingersoll Rand

Proper Use of Glycol—Coils

solution	entering fluid °F	coil rows	total capacity MBh	pressure drop (air) in. H ₂ O	fluid flow rate gpm	pressure drop (fluid) ft. H ₂ O
water	45	6	455	0.64	75.5	6.89
25% EG	45	6	395	0.62	86.4	7.83
25% EG	45	8	455	0.83	86.4	9.81
25% EG	45	6	455	0.65	120.7	14.3
25% EG	40	6	455	0.64	84.1	7.52
25% EG	38	6	455	0.64	76.8	6.41

57 | © 2011 Trane, a business of Ingersoll Rand

Upgrading Existing Chilled-Water Systems



System Design
Options

Upgrade Options

- Change the chiller
 - Retrofit
 - Replace
- Change design parameters
- Change system configuration
- Enhance controls

Design Parameters

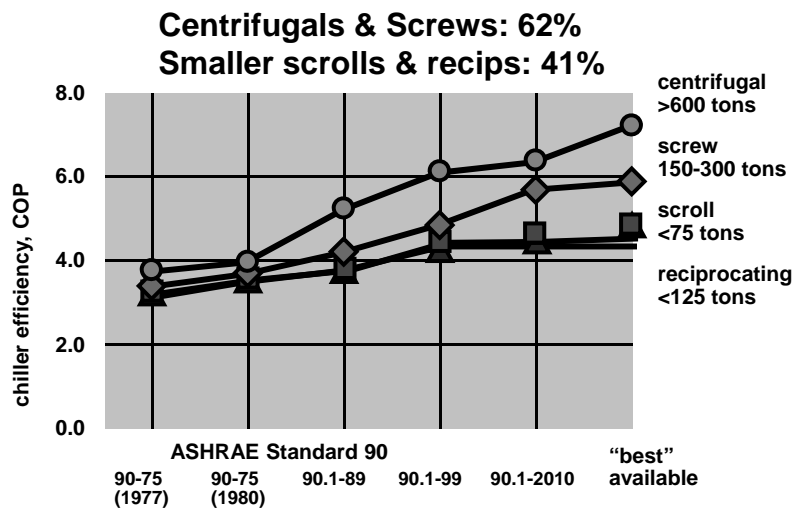
- Many chilled water systems selected at:
 - Chilled water
 - 44°F
 - 2.4 gpm/ton (10°F ΔT)
 - If water-cooled, condenser water
 - 85°F Entering
 - 3 gpm/ton (9.4°F ΔT)
- ASHRAE GreenGuide Guidance
 - Chilled water
 - 12°F to 20°F ΔT
 - 2.0 to 1.2 gpm/ton
 - Condenser water
 - 12°F to 18°F ΔT
 - 2.5 to 1.6 gpm/ton

High Performance Design Parameters

- Kelly and Chan
 - Chilled water ΔT : 18°F
 - Condenser water ΔT : 14.2°F
(3.6–8.3% energy savings in various climates)



Chiller Performance Improvements



Retrofit Applications

- Chilled water side
 - Coil
 - It's a simple heat transfer device
- $Q = U \times A \times LMTD$**
- Reacts to colder entering water by returning it warmer

63 | © 2011 Trane, a business of Ingersoll Rand

Cooling Coil Performance



MBH	504	504
EWT	44°F	41°F
GPM	101	63
GPM/ton	2.4	1.5
LWT	54°F	57°F
WTR	10°F	16°F

GPM reduction of 37.6%

64 | © 2011 Trane, a business of Ingersoll Rand

retrofit applications
Reducing Coil Water Flow Rate

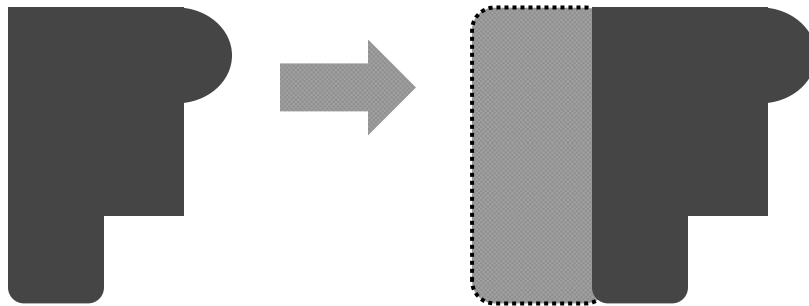
- Energy reduction
 - Pumps use less energy
 - $(1 - 0.376)^{2.5} = 0.3$
 - 70% reduction
 - Chiller energy increase offset by pump energy reduction
- System expansion
 - Existing coils use less, but colder water
 - Existing pipes and pumps can serve additional coils

$kW \rightarrow gpm^3$

$Tons = gpm \times \Delta T / 24$

Reduce Existing Coil Flow to Satisfy Flow Requirements for an Addition

- Present facility
 - 2,000 tons
 - Chilled water: 44°F, 10°F ΔT
 - 4,800 gpm
- Desired facility
 - 3,000 tons
 - Chilled water: 40°F, 16°F ΔT
 - Existing coils: 2,880 gpm
 - Coils in addition: 1,920 gpm



When Reducing Chilled Water Temperature in an Existing System, Examine

- Pipe insulation
- Existing oversized control valves
 - At lower flow rates control is poor
 - Changed valves on largest existing coils

retrofit applications

Reducing Coil Water Flow Rate

- Satisfy increased space loads
 - Existing coils use the same flow rate of colder water to satisfy increased loads

$$\text{Tons} = \text{gpm} \times \Delta T / 24$$

Condenser Side Retrofit Applications

- Situation
 - Chiller needs to be replaced
 - Cooling needs have increased by 50%
 - Cooling tower and pipes were replaced two years ago
 - Pipes run under the parking lot and nobody wants to dig them up!



69 | © 2011 Trane, a business of Ingersoll Rand

Performance with reselected chiller Same tower, condenser water pump and pipes

	Existing	38% Increase	51% Increase
Capacity (tons)	153	212	231
Flow rate (gpm)	450	450	450
Design Wet Bulb (°F)	78	78	78
Condenser Entering Water Temperature(°F)	85	87	87.6
Condenser Leaving Water Temperature (°F)	94.9	100.6	102.5
Chiller kW/ton	.837	.743	.765

70 | © 2011 Trane, a business of Ingersoll Rand

**Performance with *reselected* chiller
Same tower, condenser water pump and pipes**

	Same Capacity	38% Increase	51% Increase
Capacity (tons)	153	212	231
Flow rate (gpm)	450	450	450
Design Wet Bulb (°F)	78	78	78
Condenser Entering Water Temperature(°F)	85	87	87.6
Condenser Leaving Water Temperature (°F)	94.7	100.6	102.5
Chiller kW/ton	.679	.743	.765

71 | © 2011 Trane, a business of Ingersoll Rand

Condenser System Performance

	Existing	38% Increase	51% Increase	SAME CHILLER POWER 18% Increase
Capacity (tons)	153	212	231	180.6
Chiller kW	128.0	157.7	177.1	125.8
Tower kW	5.9	5.9	5.9	5.9
Pump kW (assume 40' of piping pressure drop)	8.6	7.3	6.9	7.9
Condenser system kW	142.5	170.9	189.9	139.6
Condenser system kW/ton	.931	.806	.822	.773

72 | © 2011 Trane, a business of Ingersoll Rand

Use the existing infrastructure to satisfy present requirements



73 | © 2011 Trane, a business of Ingersoll Rand

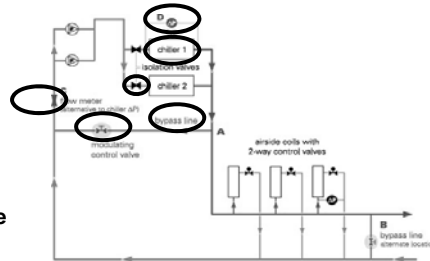
Upgrade Options

- Change the Chiller
 - Retrofit
 - Replace
- Change design parameters
- Change system configuration
- Enhance controls

74 | © 2011 Trane, a business of Ingersoll Rand

VPF System Requirements

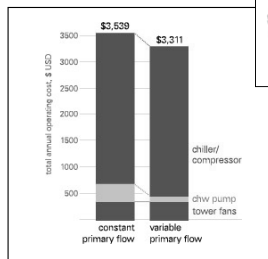
- Limits (consult manufacturer)
 - Absolute flows—minimum and maximum
- Always need a method to allow minimum flow (bypass)
- Flow rate changes
 - 2% of design flow per minute not good enough
 - 10% of design flow per minute borderline
 - 30% of design flow per minute many comfort cooling applications
 - 50% of design flow per minute best



75 | © 2011 Trane, a business of Ingersoll Rand

Why Consider Variable Primary Flow (VPF) Now?

- Chiller control sophistication
- Operating cost savings
 - Pump energy
 - Response to low ΔT Syndrome



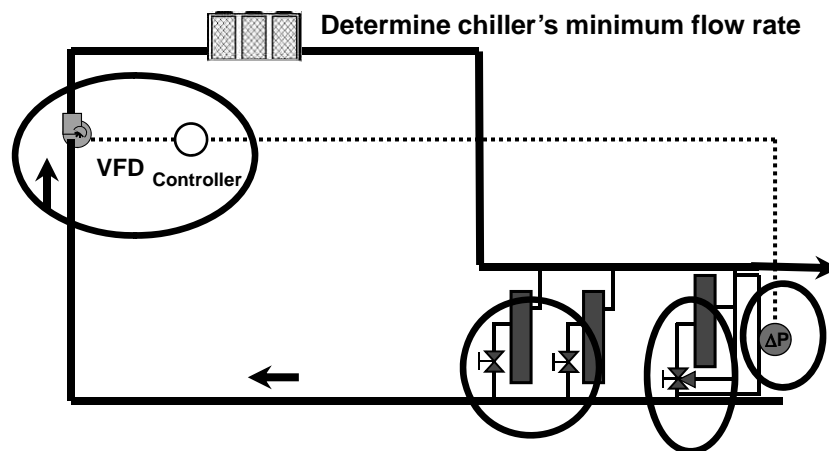
76 | © 2011 Trane, a business of Ingersoll Rand

Convert to VPF?

- Constant volume (flow) systems
 - Small
 - Large
- Primary-secondary
 - Convert by moving pumps
 - Convert by changing primary pump control

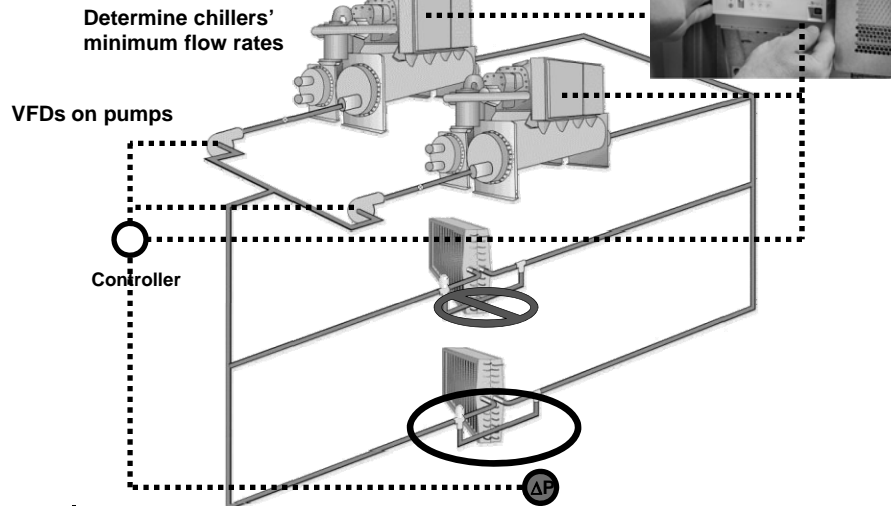
77 | © 2011 Trane, a business of Ingersoll Rand

Convert Small Constant Flow to VPF

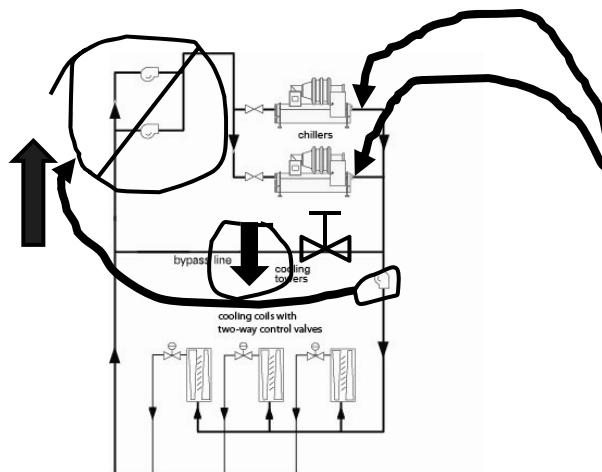


78 | © 2011 Trane, a business of Ingersoll Rand

Convert Large Constant Flow to Variable Primary Flow (VPF)



Convert Primary Secondary to Variable Primary Flow (VPF)?



Convert Primary-Secondary to VPF

Challenges of full change

- Remove primary pumps
- Secondary pumps moved
- Additional pressure drop must be satisfied by secondary pumps
- Bypass line resizing
- Flow measurement devices needed

Benefits of full change

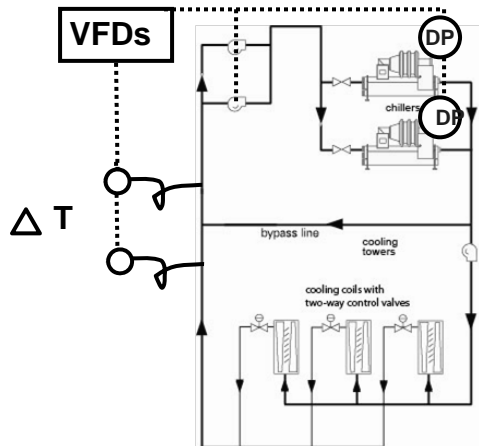
- Can now respond to “low ΔT syndrome”
- Have a true VPF system
- Frees up a lot of space
 - Can install more capacity

Letter to the Editor, HPAC July 2000

- *“...When we installed the new chillers we also converted the existing system from conventional primary-secondary to variable-volume-primary operation. When we did this we eliminated the 11 existing primary-secondary pumps and replaced them with four variable-volume-primary pumps. **Making this change allowed us to install a 1000-ton chiller in the space previously occupied by most of the 11 pumps...**”*

Colin T. Oakley, DuPage County Power Plant

Convert Primary Secondary to Variable Primary–Variable Secondary



83 | © 2011 Trane, a business of Ingersoll Rand

Convert to VPF?

- Constant volume (flow) systems
 - Small
 - Large
- Primary-secondary
 - Convert by moving pumps
 - Convert by changing primary pump control

84 | © 2011 Trane, a business of Ingersoll Rand

Upgrading Existing Chilled-Water Systems

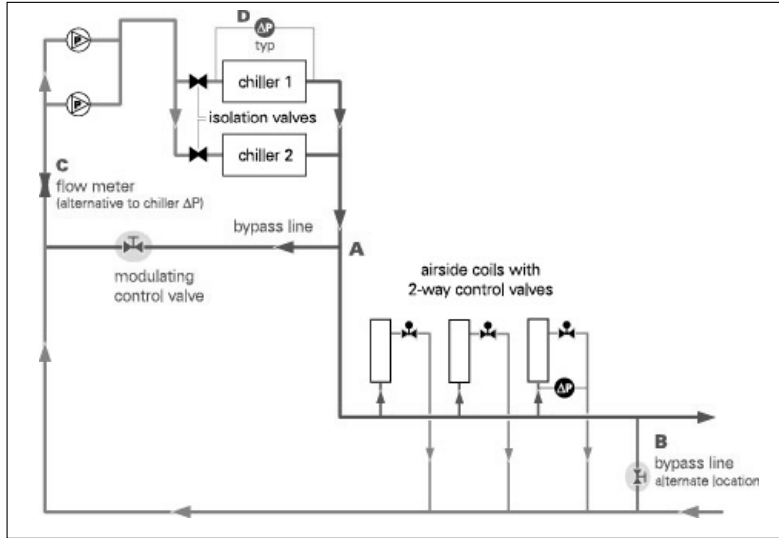


**Unit Control
Upgrades**

Onboard (Unit) Chiller Controls

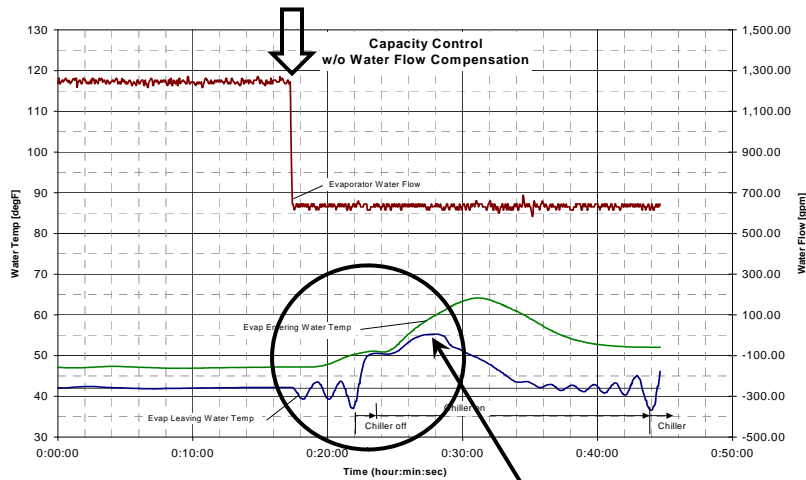
- Adapt
 - Feedback (e.G. Leaving water temperature)
 - Hold or reduce capacity (demand limit) prior to trip
 - Maximize capabilities for the conditions
 - Multiple objective limit arbitration
 - Figure out what's most dire, manage to it
 - Stay online as long as possible
- Predict
 - Feedforward (e.g. return water temperature, flow)
- Anticipate
 - Auto-tune based on flow, temperature, IGW, speed
 - Filter setpoints

Rapid Flow Rate Change



87 | © 2011 Trane, a business of Ingersoll Rand

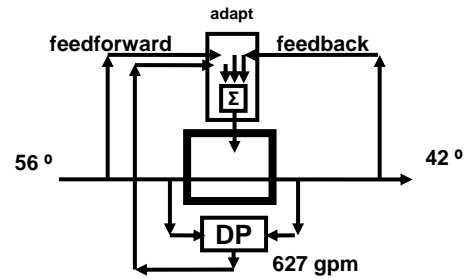
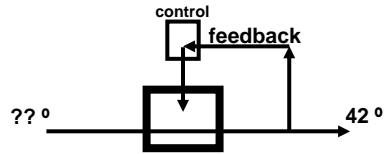
old, feedback controls 50% Flow in 30 Seconds



88 | © 2011 Trane, a business of Ingersoll Rand

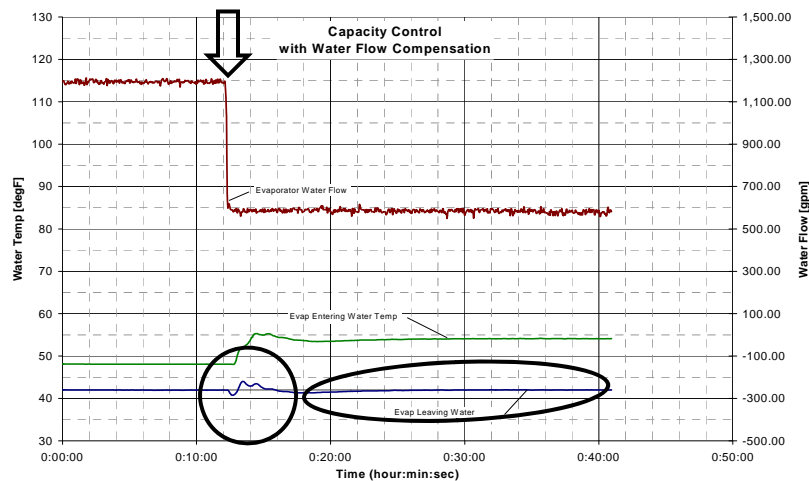
Predictive Control

- Feedback: wait until temperature is affected
- Feedforward: react *before* temperature is affected
- Auto-adjust control gains
 - Small gains for lower flow conditions
 - Aggressive gains for higher flow conditions



89 | © 2011 Trane, a business of Ingersoll Rand

compensated feed-forward 50% Flow in 30 Seconds



90 | © 2011 Trane, a business of Ingersoll Rand

VSD Control



- Simultaneously optimize speed and inlet guide vanes for optimal efficiency
- Integrated variable evaporator flow



91 | © 2011 Trane, a business of Ingersoll Rand

Summary

- Unit control upgrades
 - Many reasons to upgrade
 - Tech support
 - Parts availability/costs
 - If going to VPF your control must be capable

92 | © 2011 Trane, a business of Ingersoll Rand

For More Information on VPF

- <http://trane.com/commercial/library/newsletters.asp> (1999 and 2002)
- “Primary-Only vs. Primary-Secondary Variable Flow Systems,” Taylor, ASHRAE Journal, February 2002
- “Don’t Ignore Variable Flow,” Waltz, Contracting Business, July 1997
- “Comparative Analysis of Variable and Constant Primary-Flow Chilled-Water-Plant Performance,” Bahnfleth and Peyer, HPAC Engineering, April 2001
- “Campus Cooling: Retrofitting Systems,” Kreutzmann, HPAC Engineering, July 2002

93 | © 2011 Trane, a business of Ingersoll Rand

Upgrading Existing Chilled-Water Systems



System Controls

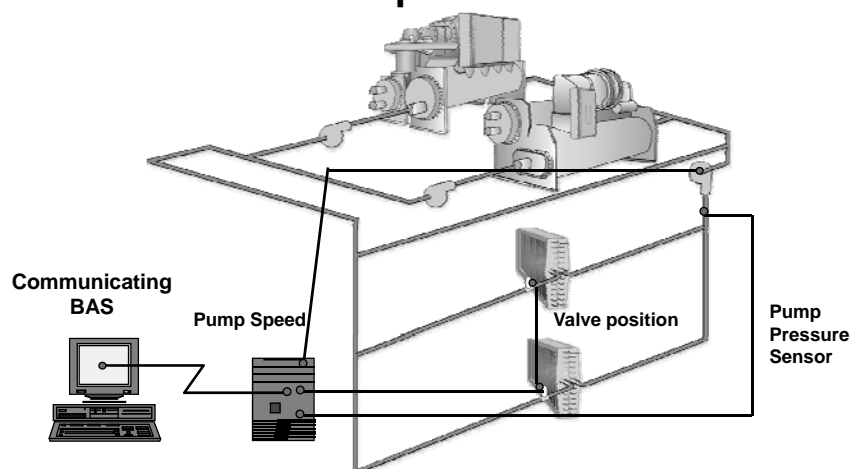
System Controls

- Pump pressure optimization
- # of chillers to operate
- Chiller-tower optimization
- # of towers to operate
- Variable condenser flow



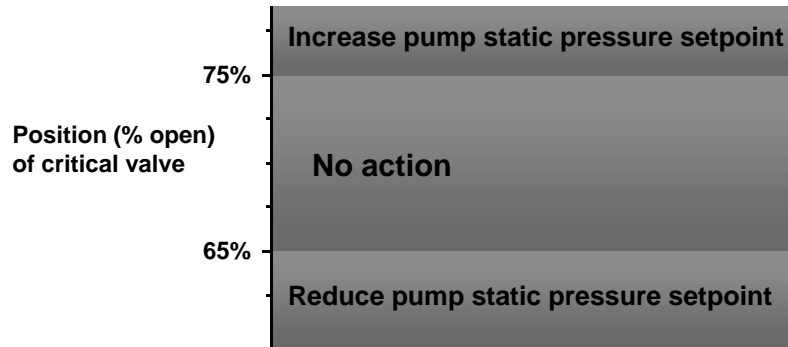
95 | © 2011 Trane, a business of Ingersoll Rand

Chilled Water Pump Control



96 | © 2011 Trane, a business of Ingersoll Rand

Pump-Pressure Optimization



Required for DDC systems by 90.1-2010

97 | © 2011 Trane, a business of Ingersoll Rand

Number of Chillers to Operate

- Operate one at nearly full load or two at part load?
- Examine IPLV assumptions

98 | © 2011 Trane, a business of Ingersoll Rand

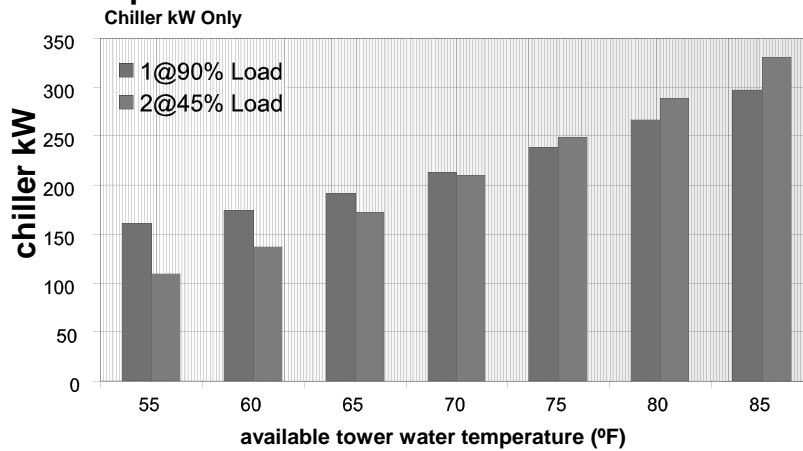
VSDs and centrifugal chillers A Closer Look at IPLV

Load	Weighting		kW/Ton
100%	0.01		0.572
75%	0.42		0.420
50%	0.45		0.308
25%	0.12		0.372

VSDs improve part-load performance, so running two chillers with VSDs at part load seems more efficient than one chiller at double the same load, but ...is dependent on condenser water temperature

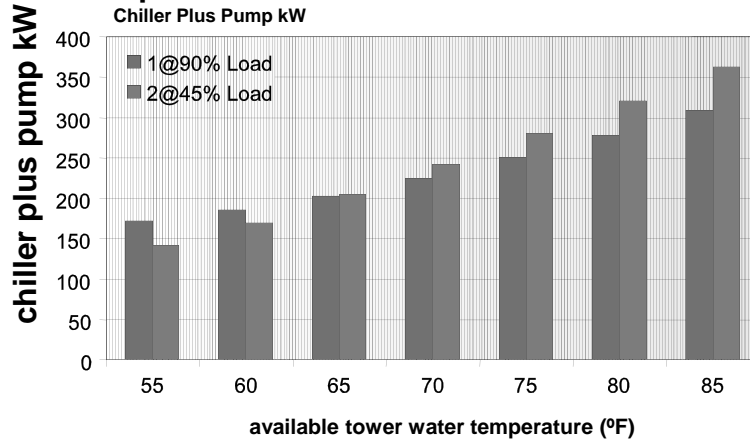
chiller power only 45% Plant Load

Operate 1 or 2 chillers?



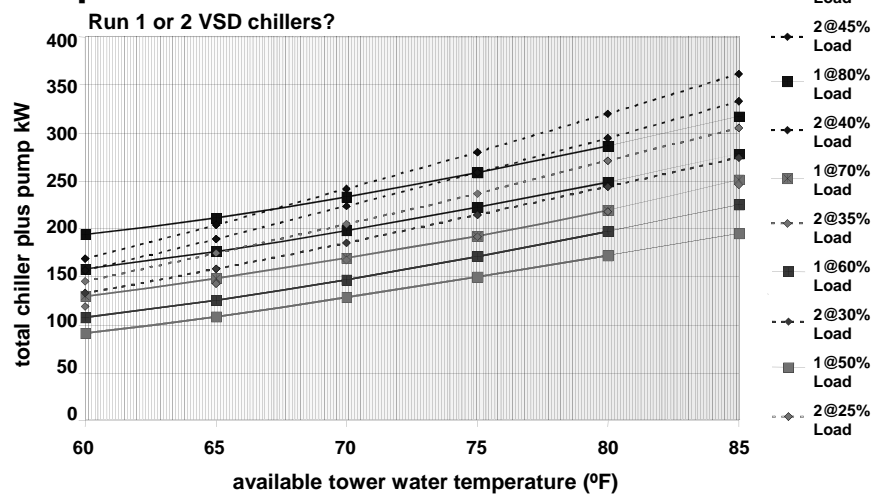
chillers plus pumps 45% Plant load

Operate 1 or 2 Chillers?



101 | © 2011 Trane, a business of Ingersoll Rand

Operate 1 or 2 Chillers?



102 | © 2011 Trane, a business of Ingersoll Rand

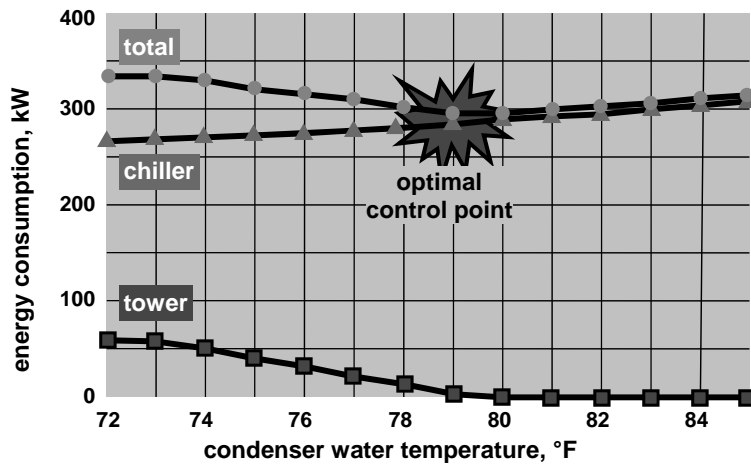
Operate 1 or 2 Chillers?

- 45% plant load: one chiller until tower temperature is < 65°F
- 40% plant load: one chiller until tower temperature is < 60°F
- 35% plant load and below: one chiller

chiller-tower optimization Documentation

- Braun, Diderrich: ASHRAE Transactions (1990)
- Schwedler, Hage, Dorman, Stiyer (1993)
- Schwedler: ASHRAE Journal (July 1998)
- Hydeman, Gillespie, Kammerud:
PG&E CoolTools™ program (2000)
- Cascia: ASHRAE Transactions (2000)
- Crowther, Furlong: ASHRAE Journal
(July 2004)

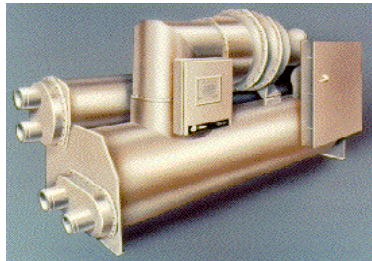
optimal condenser water control Chiller-tower Interaction



105 | © 2011 Trane, a business of Ingersoll Rand

chiller-tower optimization Dependent On?

- Chilled water plant
 - Tower design
 - Chiller design
 - Centrifugal
 - Helical rotary
 - Variable speed drive
 - Absorption
 - Changing conditions
 - Chiller load
 - Ambient wet bulb



106 | © 2011 Trane, a business of Ingersoll Rand

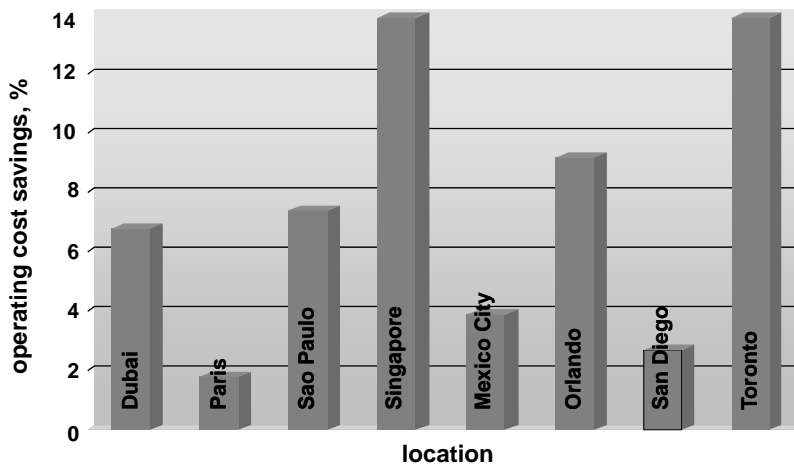
chiller-tower optimization Estimated Savings

- Crowther & Furlong
("Optimized" vs. driving water to 65°F)
 - Chicago: 5.4%
 - Las Vegas: 2.6%
 - Miami: 8.5%

Based on chiller+tower annual energy consumption

107 | © 2011 Trane, a business of Ingersoll Rand

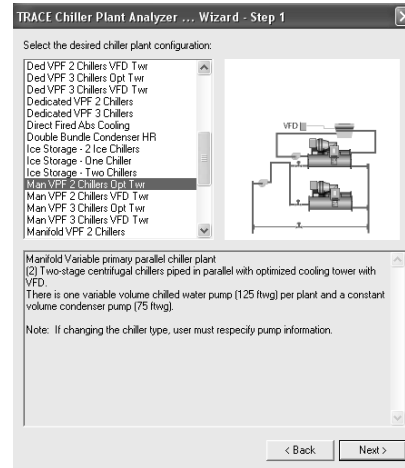
chiller-tower optimization Operating Cost Savings



108 | © 2011 Trane, a business of Ingersoll Rand

chiller-tower optimization How Do You Calculate Savings?

- TRACE Chiller Plant Analyzer
- System Analyzer™
- TRACE® 700



How Many Cooling Tower Cells Should Be Operated?

- For this discussion: assume condenser water pump speed is constant
- Simple answer: as many as allowable
 - More heat exchange surface
 - Closer tower approach temperature
 - Lower airflow to achieve tower setpoint
 - Reduced airflow = lower tower fan power

example
Operating More Cooling Tower Cells

- Design conditions
 - Two 500-ton chillers
 - Each
 - 1000 gpm condenser water flow rate
 - Two tower cells (each)
 - 99/85/78
 - 40 hp
- Operating conditions
 - 200 ton load
 - One chiller
 - Condenser water flow rate: 1000 gpm
 - Condenser water ΔT : 5.6°F

example
Operating More Cooling Tower Cells

	One cell	Two Cells
Total flow (gpm)	1000	1000
Flow per cell (gpm/cell)	1000	500*
Tower setpoint (°F)	65	65
Wet bulb temperature (°F)	60	60
Approach (°F)	5	5
Range (°F)	5.6	5.6
Fan speed (%)	100%	39 %
Total fan power (bhp)	40.0	23.4
Tower fan power savings (bhp)	0	16.6

***Stay above tower cell minimum water flow rate**

issues

Reducing Tower Cell Water Flow Rates

- Poor water distribution over the tower fill
- Dry spots in the cooling tower
 - Poor heat transfer
- Scale on fill
 - Poor heat transfer
 - Increased maintenance
- During winter, icing concerns

VSD on the Condenser Water Pump

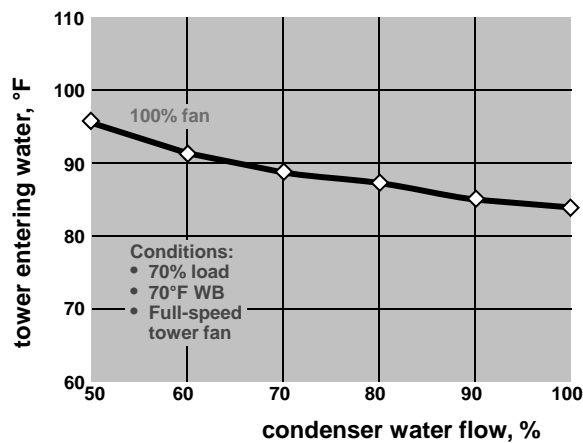
- Ensure pump motor is compatible with a drive
- Balance the flow
 - Open triple duty valve
 - Set pump speed to balance to design flow
 - Save condenser water pump energy
- Use the VSD for head pressure control
- Vary condenser water flow?
 - Savings are possible
 - It's complicated
 - Minimum pump speed

VSD on the Condenser Water Pump

- Pump minimum speed dependent on one of the following
 - Minimum allowable chiller condenser flow
 - maintain good heat transfer and control
 - Minimum speed to achieve tower static lift
 - Open portion of condenser loop, from the tower sump to the top of the tower
 - Minimum allowable tower water flow
 - Maintain proper distribution over fill
 - » Avoid dry spots in tower
 - » Reduce possibility of scaling
 - » Maintain good heat transfer
- CONFIRM WITH TOWER PROVIDER!**

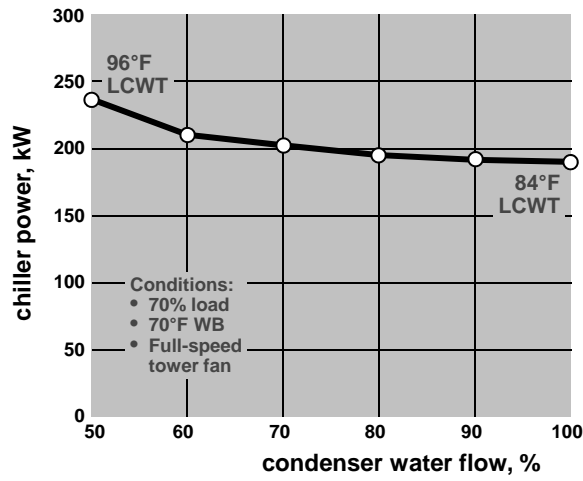
115 | © 2011 Trane, a business of Ingersoll Rand

variable condenser water flow Effect on Tower



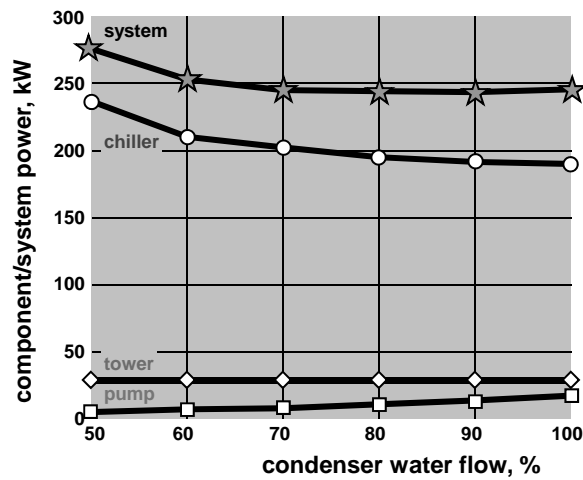
116 | © 2011 Trane, a business of Ingersoll Rand

variable condenser water flow Effect on Chiller



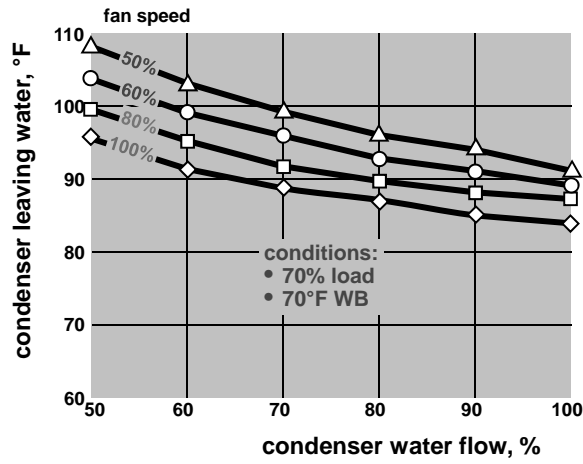
117 | © 2011 Trane, a business of Ingersoll Rand

variable condenser water flow Effect on System



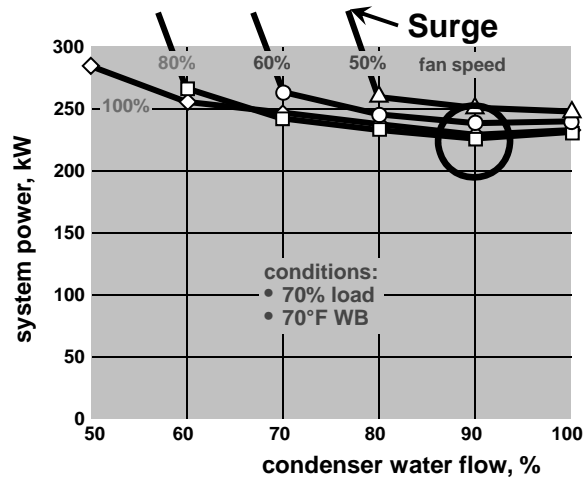
118 | © 2011 Trane, a business of Ingersoll Rand

reducing flow & fan speed Effect on Tower



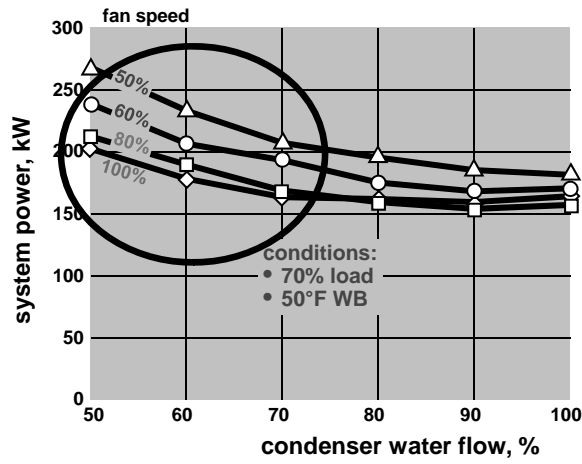
119 | © 2011 Trane, a business of Ingersoll Rand

reducing flow & fan speed Effect on System



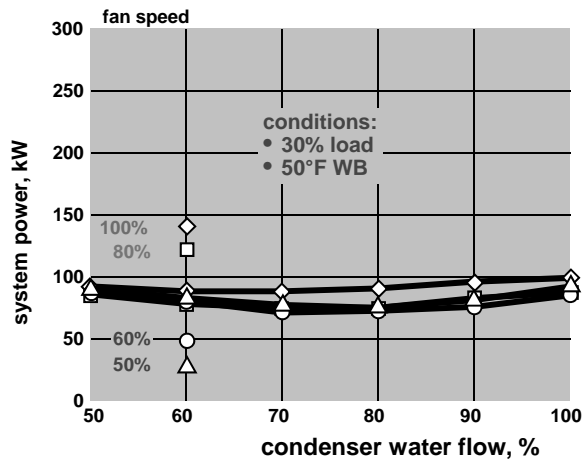
120 | © 2011 Trane, a business of Ingersoll Rand

reducing flow & fan speed Effect on System



121 | © 2011 Trane, a business of Ingersoll Rand

reducing flow & fan speed Effect on System



122 | © 2011 Trane, a business of Ingersoll Rand

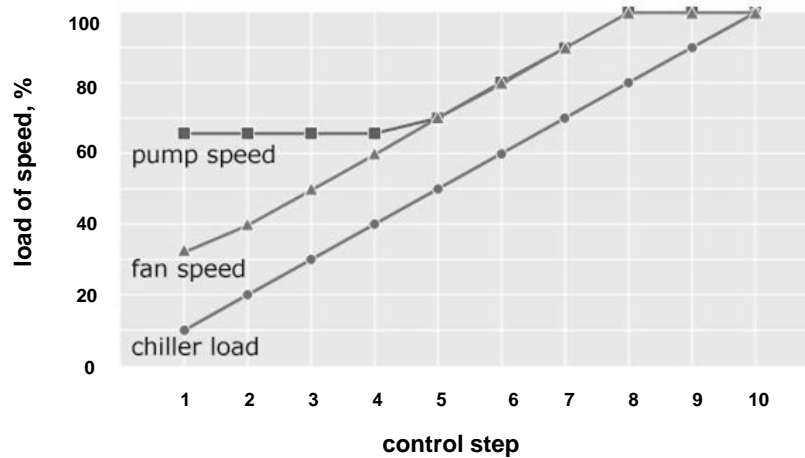
Varying Condenser Water Flow and Cooling Tower Fan Speed

% Chiller Load	Outdoor Wet Bulb Temperature (°F)	Condenser Water Pump Speed (%)	Cooling Tower Fan Speed (%)
70	70	90	90
70	50	90	80
30	50	70	60

- These are only three points in time
- What about the rest of the year?

123 | © 2011 Trane, a business of Ingersoll Rand

Varying Fan and Pump Speed Together



124 | © 2011 Trane, a business of Ingersoll Rand

variable condenser water flow
Summary

Determine what savings, if any, are possible

- Are pumps already low power?
- Can reducing tower-fan speed achieve most of the savings?

variable condenser water flow
Summary

If you decide to reduce flow:

- Find minimum condenser-water flow rate
- Examine system at various loads and wet-bulbs, as well as chiller/tower combinations
 - keep chiller out of surge
- Document the sequence of operation
- Help commission the system

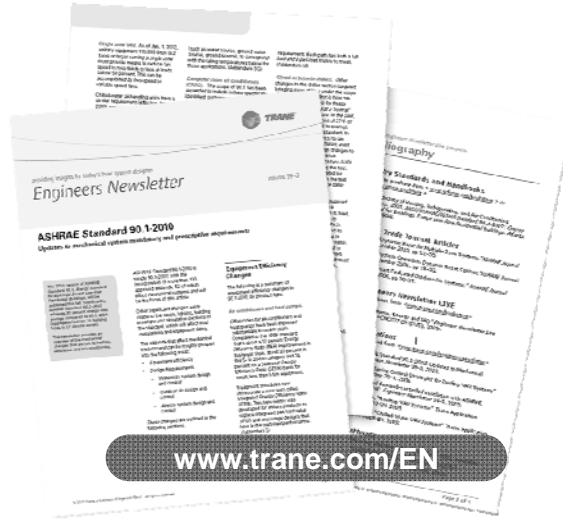
variable condenser water flow
Guidance

- Can provide savings
 - Finding proper operating points requires more time, more fine-tuning
- Two-step process:
 1. Reduce design pump power
 2. Is variable condenser-water flow still warranted?

References

- Schwedler, “*Upgrading Chilled-Water Systems,*” *ASHRAE Journal*, November 2009
- Baker, Roe, Schwedler, “*Prescription for Chilled Water Plants,*” *ASHRAE Journal*, June 2006.

references for this broadcast
Where to Learn More



129 | © 2011 Trane, a business of Ingersoll Rand

watch past broadcasts
www.trane.com/enl



- Insightful topics on HVAC system design:
 - Chilled-water plants
 - Air distribution
 - Refrigerant-to-air systems
 - Control strategies
 - Industry standards and LEED
 - Energy and the environment
 - Acoustics
 - Ventilation
 - Dehumidification



130 | © 2011 Trane, a business of Ingersoll Rand

Continuing Education

CONTINUING EDUCATION COURSES (USGBC, AIA)

ASHRAE Standards 62.1 and 90.1, and VAV Systems

- Key VAV system requirements found in both standards
- How to avoid the potential conflict between the central reheat restrictions of Standard 90.1 and dehumidification requirements of Standard 62.1
- How to choose VAV box minimum airflow settings to avoid the potential conflict between the local reheat restrictions and the minimum ventilation at all loads
- How implement zone-level demand controlled ventilation to save energy while maintaining minimum ventilation

Video 1 of 9

TraneENL_ASHRAE Standards 62.1 and 90.1 and V

Today's Presenters



Dennis Stanke staff applications
Mick Schwedler manager
Steve Taylor principal

www.trane.com/ContinuingEducation

- Earn an average of 1.5 learning units
- New courses added monthly
- Topics include:
 - Central Geothermal Systems
 - ASHRAE Standards
 - Ice Storage
 - Industry standards and LEED
 - Energy and the environment



Engineers Newsletter Live 2011

- **June**
 - High Performance VAV Systems
- **October**
 - Dedicated Outdoor Air Units

Upgrading Existing Chilled-Water Systems

